

RF Kicker for Head-on-Collision

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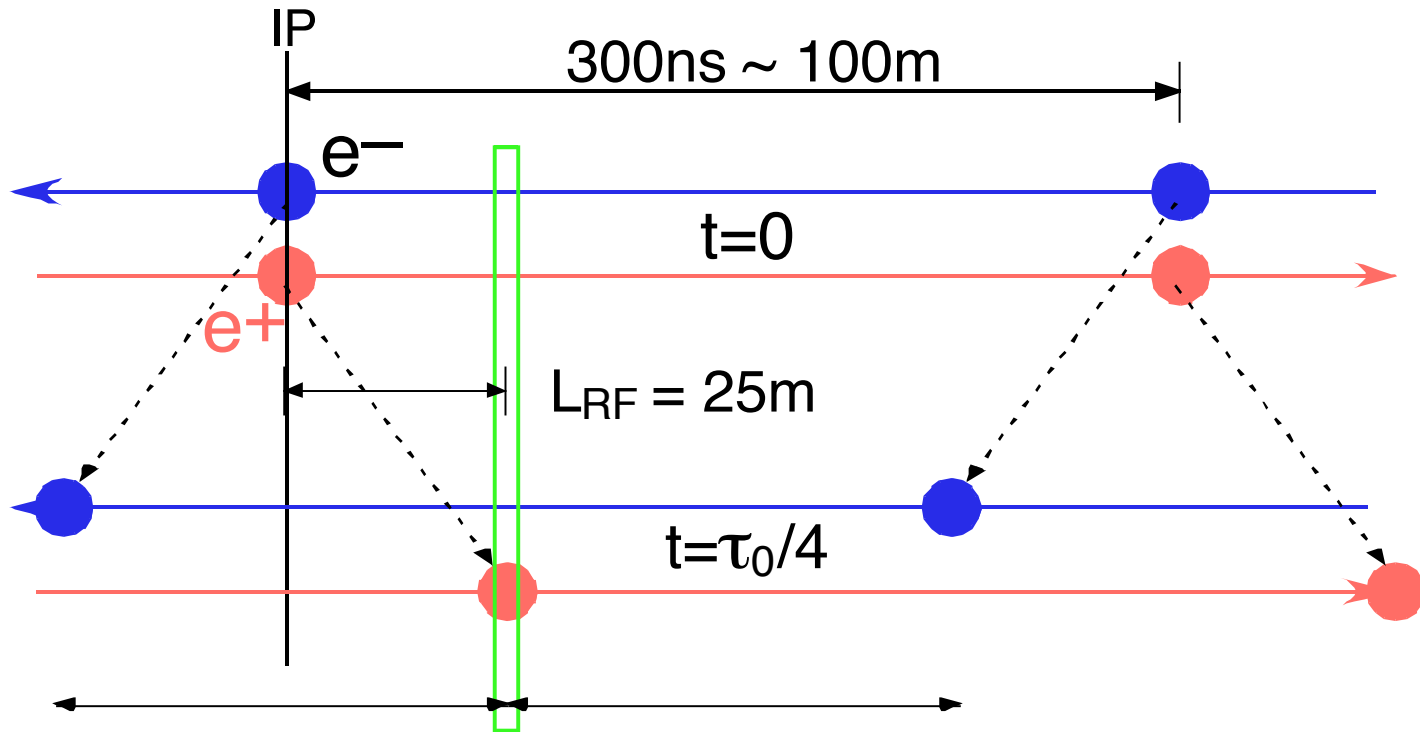
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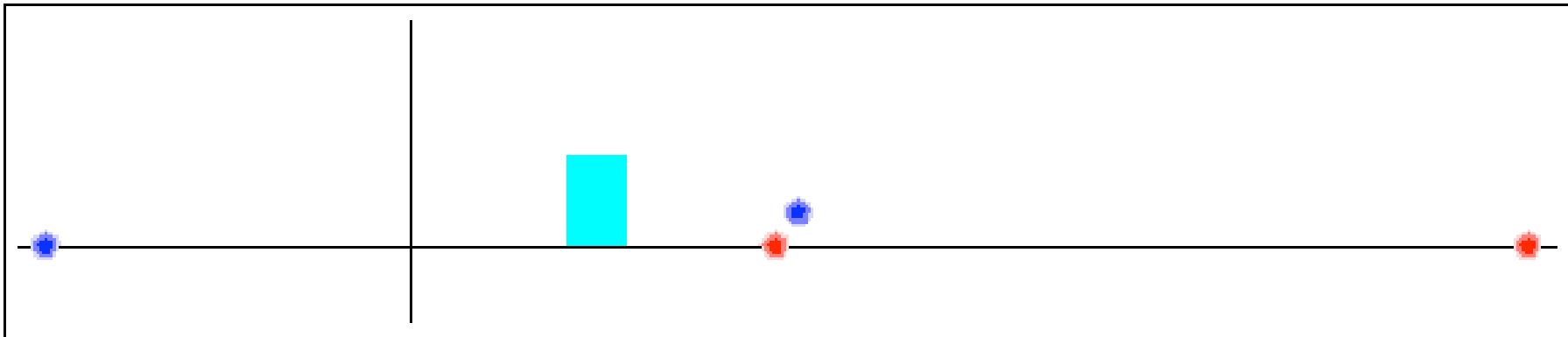
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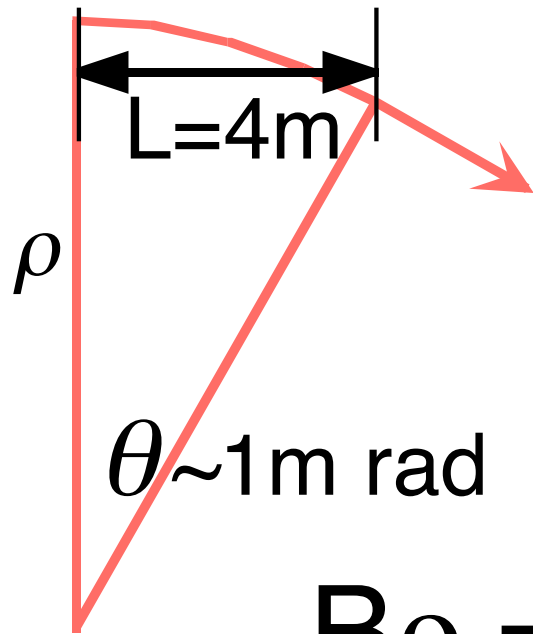
Time Structure of Beam



Out-bunch at the Center of In-bunch



Magnetic Field Strength



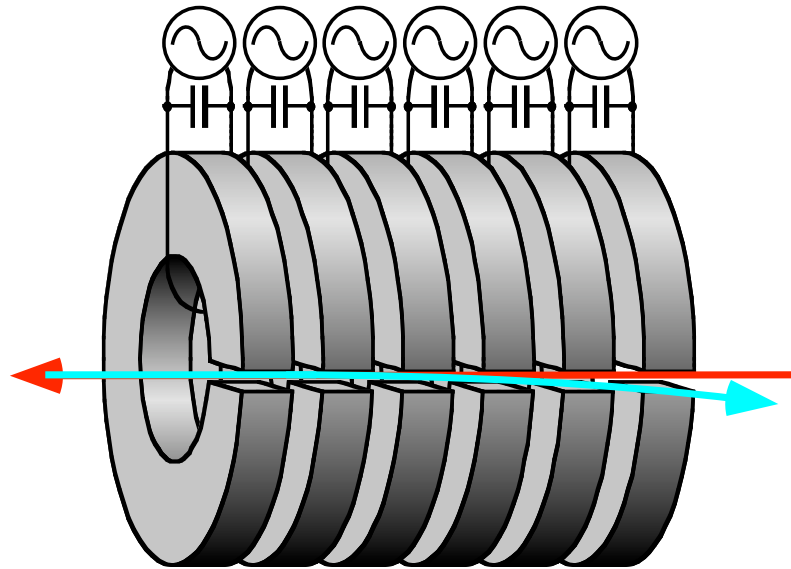
$$B\rho = \sim 1 \text{ T.km @ } 250\text{GeV}$$

$$\rho = L(4\text{m})/\theta(1\text{mrad})=4\text{km}$$

$$B=0.25\text{T}$$

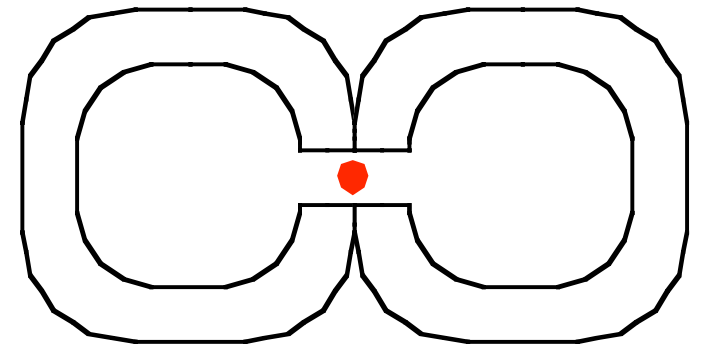
Sketch of a Kicker

DC+3MHz (+9MHz)



$L=4\text{m}$

Variant



Double C-type

Better shielding

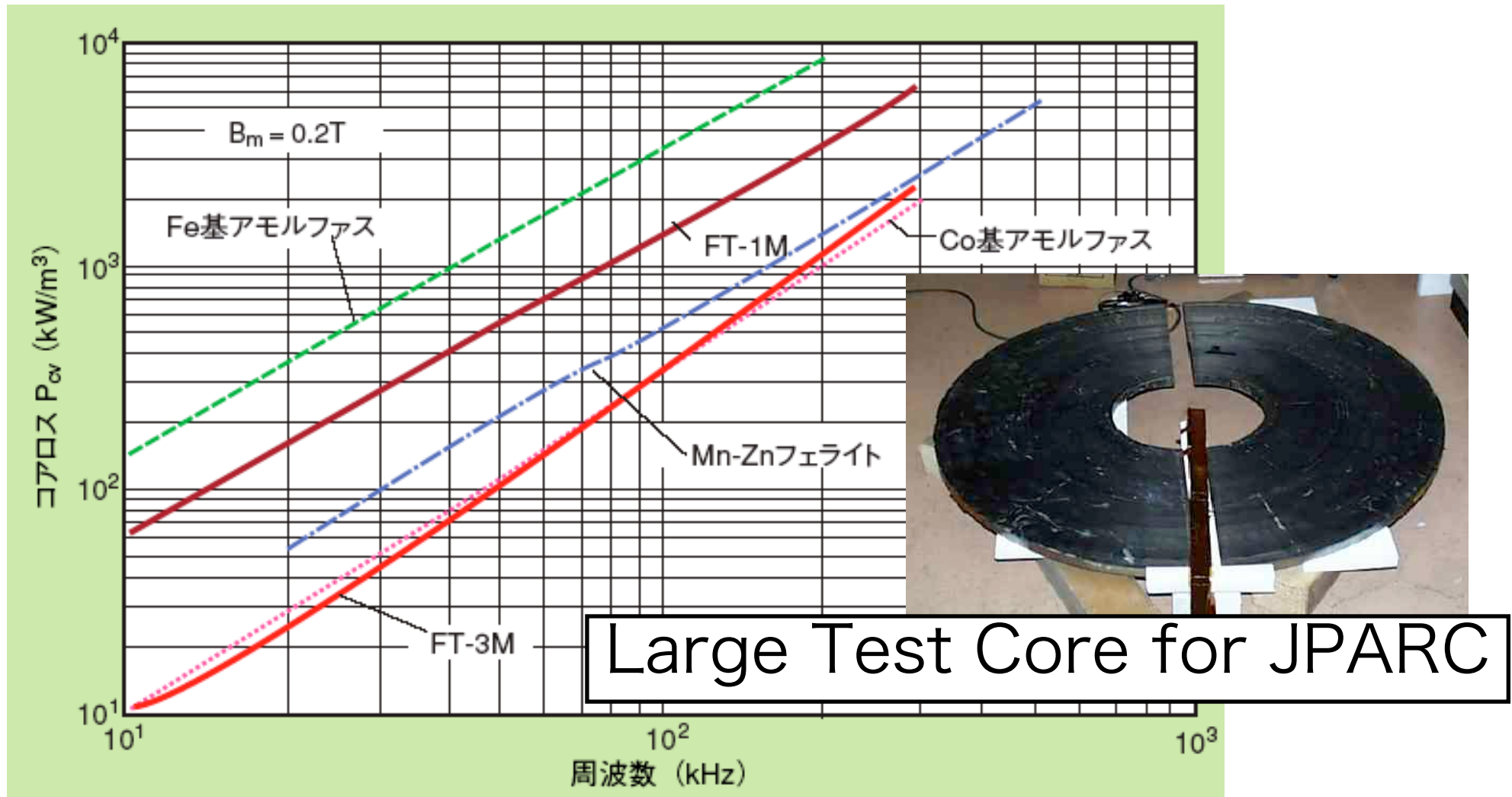
Step at center?

Stored Energy $W \sim 125[\text{J}] @0.25\text{T}$

$\times 3\text{MHz}/Q(\sim 100?)/(4\text{m}/3\text{cm}) \sim 35\text{kWpk}$

($\times 133$ units $\rightarrow 4.5\text{MWpk}$ in total)

Magnetic Alloy (Finemet)



$Q < 1$ for non-cut core

$Q \sim 10$ for cut core @ a few mm gap

Table 2. Electrical Characteristics of FINEMET® FT-1H Core

	ΔB (T)	Core loss(J/m ³) *
FINEMET® FT-1H	1.76	1000
Fe-based Amorphous	2.04	1800
Ni-Zn Ferrite	0.65	160

*Pulse width=0.5 μ sec

High B, low core loss

FT-3L

【ファインメット®と従来材の磁気特性（ノーカット・トロイダルコア）】

材 料		板厚 (μm)	B_s (T)	B_r/B_s (%)	H_c (A/m)	$\mu_r(1\text{kHz})$ ($\times 10^3$)	$\mu_r(100\text{kHz})$ ($\times 10^3$)	P_{cv} (kW/m^3)	λ_s ($\times 10^{-6}$)	T_c ($^{\circ}\text{C}$)
ファインメット®	FT-1H	18	1.35	90	0.8	5.0	1.5	950	+ 2.3	~570
	FT-1M		1.35	60	1.3	70.0	15.0	350		
	FT-3H	18	1.23	89	0.6	30.0	5.0	600	≈ 0	~570
	FT-3M		1.23	50	2.5	70.0	15.0	300		
	FT-3L		1.23	5	0.6	50.0	16.0	250		
Fe基アモルファス		25	1.56	83	2.4	5.0	5.0	2200	+ 27	415
Co基アモルファス高透磁率材		18	0.55	5	0.3	115.0	18.0	280	≈ 0	180
Co基アモルファス高角形比材		18	0.60	85	0.3	30.0	10.0	460	≈ 0	210
3%Siケイ素鋼		50	1.90	85	6.0	2.7	0.8	8400	- 0.8	750
6.5%Siケイ素鋼		50	1.30	63	45.0	1.2	0.8	5800	- 0.1	700
50%Niパーマロイ		25	1.50	95	12.0	—	—	3400	+ 25	500
80%Niパーマロイ高透磁率材		25	0.74	55	0.5	50.0	5.0	1000	≈ 0	460
80%Niパーマロイ高角形比材		25	0.74	80	2.4	—	—	1200	≈ 0	460
Mn-Znフェライト高透磁率材		—	0.44	23	8.0	5.3	5.3	1200	- 0.6	> 150
Mn-Znフェライト低損失材		—	0.49	29	12.0	2.4	2.4	680	- 0.6	> 200

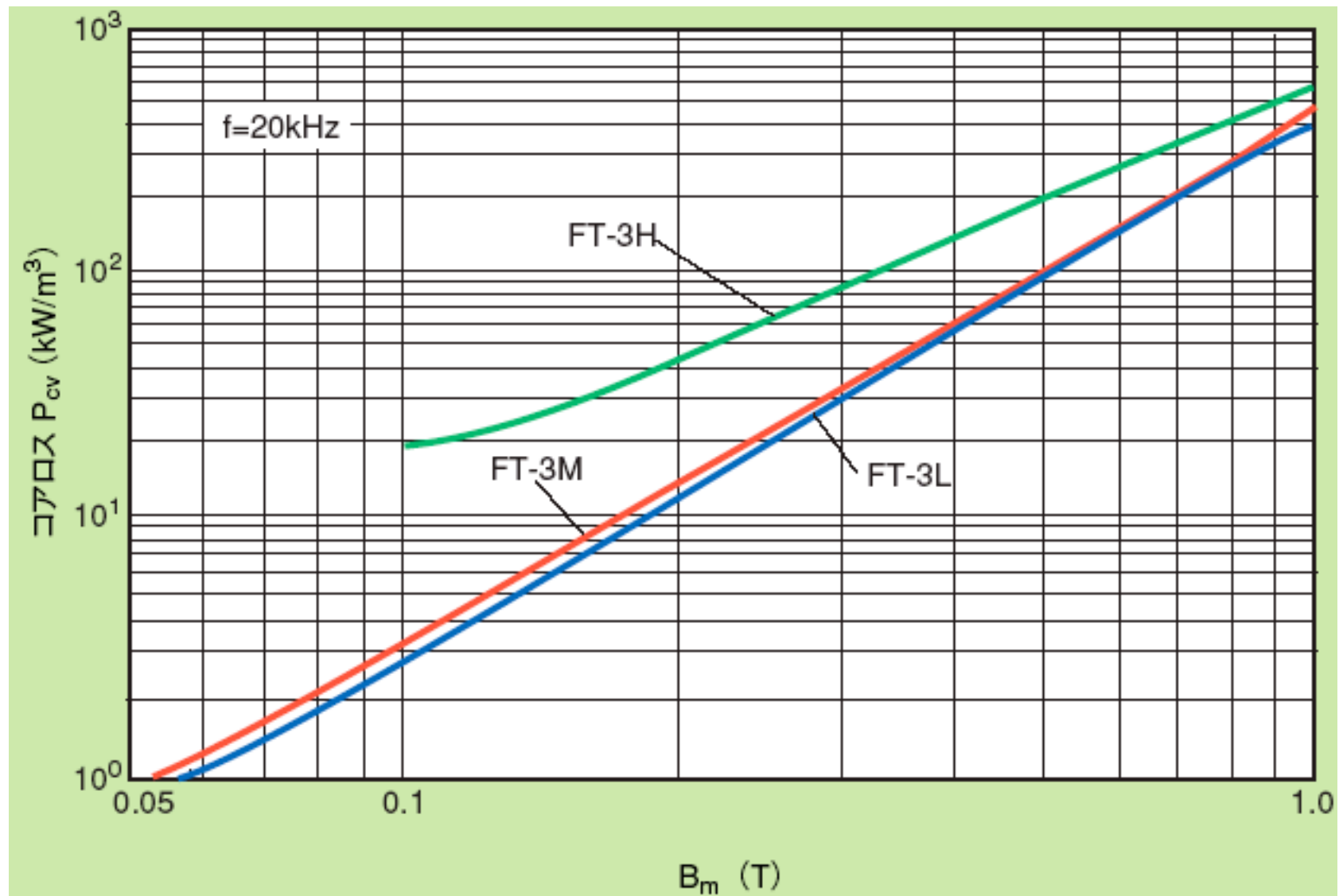
注1) $B_s, B_r/B_s, H_c$: 直流磁気特性 ($H_m=800\text{A}/\text{m}$, 25°C)、 $\mu_r(1\text{kHz})$: 比透磁率 (1kHz, $H_m=0.05\text{A}/\text{m}$, 25°C)、

$\mu_r(100\text{kHz})$: 比透磁率 (100kHz, $H_m=0.05\text{A}/\text{m}$, 25°C)、 P_{cv} : コアロス (100kHz, $B_m=0.2\text{T}$, 25°C)、 λ_s : 飽和磁歪定数、 T_c : キュリー温度

注2) 上記特性は、当社での測定による

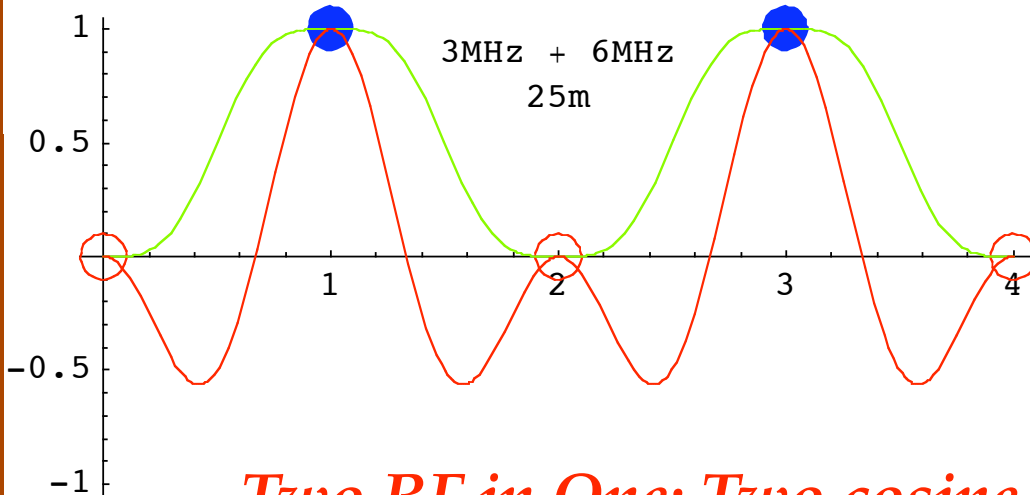
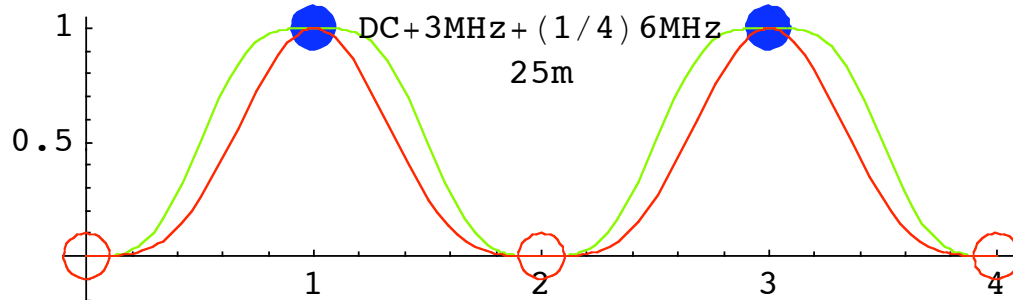
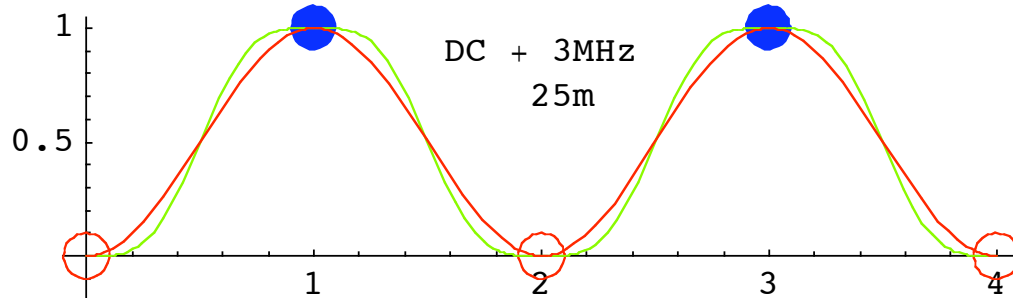
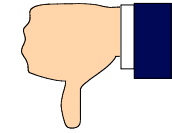
High B, low core loss, high Tc

Core Loss



FT-3L is the best option here.

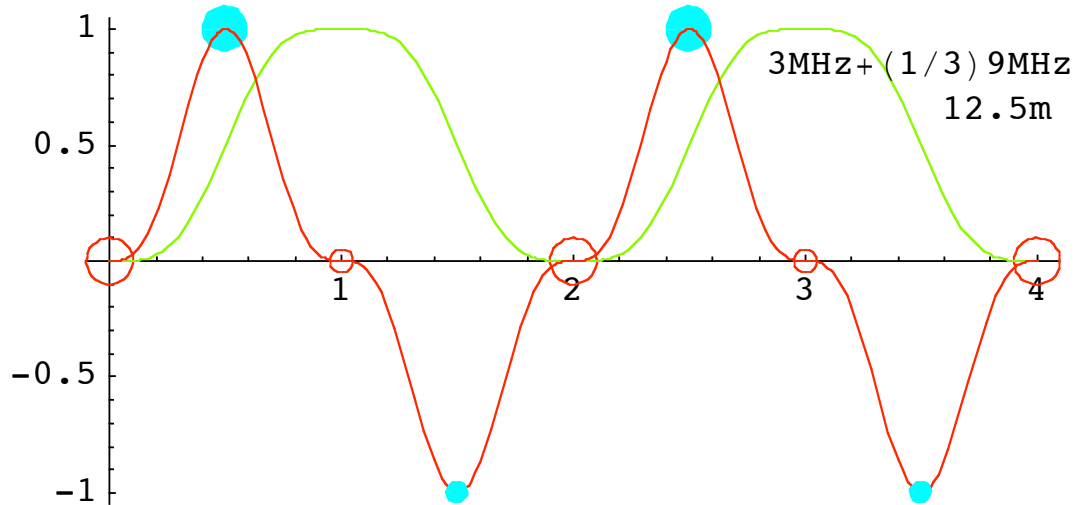
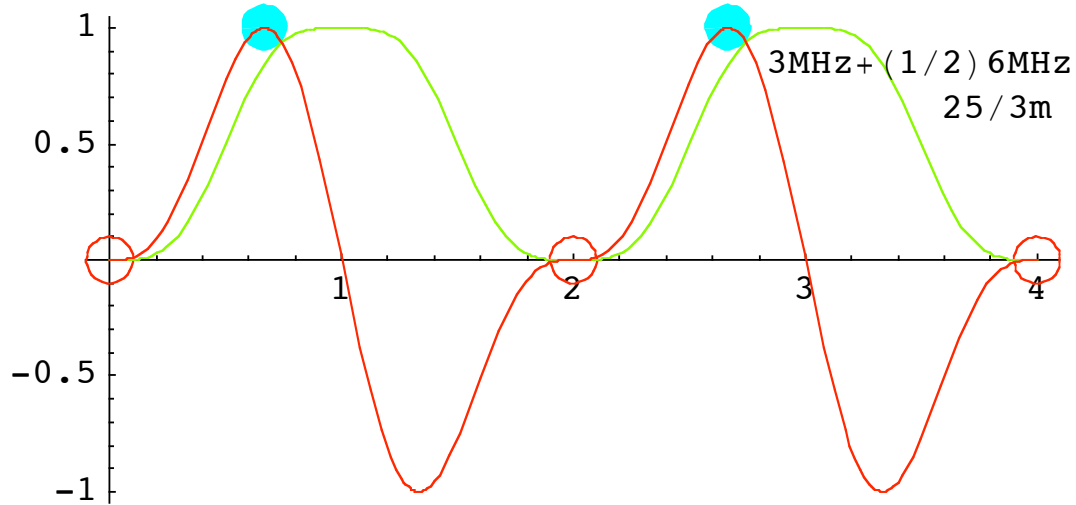
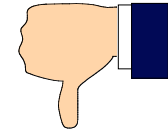
Waveforms-1



Single RF	needs DC
Wide Base	needs DC Two RF in One
No DC	Narrow Base Two RF in One

Two RF in One: Two cosine components superposition

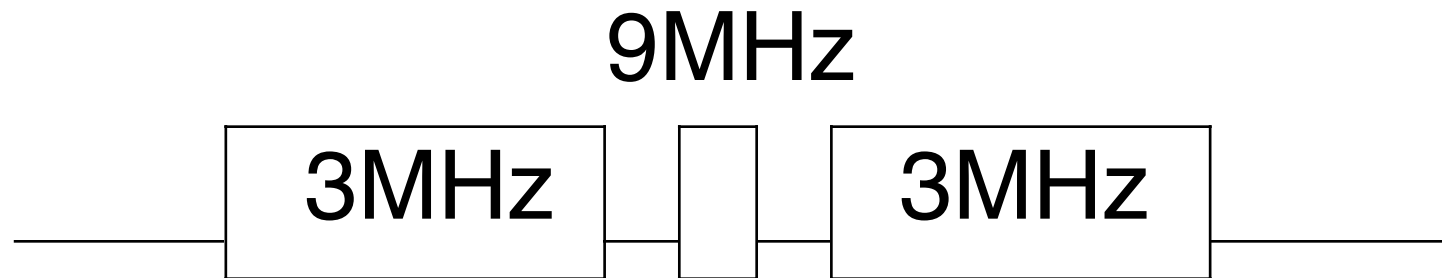
Waveforms-2



<p>No DC Separate RF</p>	<p>Short LRF Two RF</p>
<p>No DC Separate RF 6MHz too (if 2 sides OK)</p>	<p>Short LRF Two RF</p>

Separate RF: Each component for each separate kicker

Combination



- Separate two RF system for the latter two options.
- Phase slip for in-bunch can be compensated by phasing.
—> less perturbation

Comments

- MA has been used for RF accelerating cavity to generate high voltage ($V = \dot{\Phi} = \dot{B}S$).
→ Not for generation of B. (R&D!)
- Estimated RF power:
~4.5MWpk, 23kWave. (.25Tx4m, 1m rad)
35kW x (133 cores, 133 Amp's)
- Upgradable to 1TeV(6MHz) — Two sets?
- Easier than Crab-cavity